	Evaluation Report
Project	21855_2 – Condensed version Injection System WIT-VM 250 for masonry – resistance to fire
Client	Adolf Würth GmbH & Co. KG Reinhold Würth Straße 12-17 74653 Künzelsau
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### 1 General information

Adolf Würth GmbH & Co. KG authorized the evaluation of the fire resistance of the chemical anchor system WIT-VM 250 for axial tension and shear loads. The evaluation concerning steel strength and pullout resistance carried out in dependence on section 2.3 of Technical Report 020 [1]. The evaluation is based on tests that were conducted by the Technical University Kaiserslautern under fire exposure according to DIN EN 1363-1:2012 [2]. The test results are summarized in test reports 16030CT/15511 [3] and 18036MR/15561 [4].

This evaluation provides fire resistances which covers anchors with fire attack from one side only.

#### 2 Reference documents

- [1] Evaluation of Anchorages in Concrete Concerning Resistance to fire, EOTA TR 020, Edition May 2004
- [2] Feuerwiderstandsprüfungen Teil 1: Allgemeine Anforderungen, DIN EN 1363-1; Edition Oktober 2012
- [3] Test Report 16030CT/15511, March 2017, deposited at Ingenieurbüro Thiele
- [4] Test Report 18036MR/15561, August 2018, deposited at Ingenieurbüro Thiele
- [5] European Technical Assessment ETA-16/0757 for Injection system WIT-VM 250 +SH or WIT-Nordic + SH for masonry, EOTA, 15 December 2016
- [6] Guideline for European Technical Approval of Metal Injection Anchors for Use in Masonry, EOTA ETAG 029, April 2013

### 3 Product description

The WIT-VM 250 is a bonded anchor system consisting of a plastic cartridge containing the injection mortar and a steel part. For usage in hollow bricks also a perforated sleeve is part of the system.

The injection system WIT-VM 250 is designed for the use masonry according to the European Technical Approval ETA-16/0757.

### 4 Scope of evaluation

The present evaluation of the fire resistances of the injection system WIT-VM 250 in masonry is assessed with respect to its fire resistance properties as anchor applications in walls. The tests which this evaluation refers to, are executed with horizontal arranged

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anchors and axial load application. Furthermore the anchors were exposed to the standard temperature-time curve (ETK) [2]. In the tests a fixture according to TR020 was used, therefore the following fire resistances cover only anchors protected from fire by attachments similar to the fixture according to TR020 [1].

The assessment is carried out in dependence on TR020 [1]. Divergent test results of all types of failure (steel failure, pullout failure) are assessed together.

a. Steel failure:

No additional tests for the assessment of steel failure are necessary because the resulting fire resistances are smaller and values with steel failure are assessed together. Threaded rods with a minimum steel grade of 5.8 shall be used. The evaluation covers threaded rods made of stainless steel as well.

b. Pullout failure:

Most results deliver pullout failure in the fire tests.

c. Brick failure:

In the fire tests evaluated in this document no absolute brick breakout failure could be observed. Therefore it was suggested that this failure type has no influence on the fire resistances of the anchor system WIT-VM 250.

In hollow bricks the worse position in brick was tested, so that the fire resistances which are given in the following covers all positions in a hollow brick.

The fire resistances which are given in chapter 5 covers axial loads and shear loads as well. The evaluation is performed for the brick types given in ETA-16/0757 [5]. According to ETAG 029 [6], the results in Table 5-1 can also be transferred to solid brick types with higher strength and larger dimensions.

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#### 5 Summary

Table 5-1 shows the fire resistances for the use of anchor system WIT-VM 250 in the proved undergrounds. The given fire resistances covers axial and radial loads.

Characterstic resistance against pullout/steel failure										
Brick type	Anchor size	Minimum anchorage depth	Perforated sleeve	R30	R60	R90	R120			
[-]	[mm]	[mm]	[mm x mm]	[kN]	[kN]	[kN]	[kN]			
	8	80		1,05	0,80	0,55	0,45			
clay (Mz) solid brick	10	90		2,10	1,60	1,05	0,80			
	12	100		3,50	2,55	1,60	1,10			
	16	100		4,70	3,25	1,80	1,05			
	8	80		1,05	0,80	0,55	0,45			
sand lime (KS)	10	90		2,10	1,60	1,05	0,80			
solid brick	12	100		3,50	2,55	1,60	1,10			
	16	100		4,70	3,25	1,80	1,05			
	8	80		1,20 (1,35) <sup>1)</sup>	0,85	0,35	0,10			
aerated	10	90		1,70	1,15	0,65	0,35			
concrete	12	100		2,05	1,45	0,90	0,60			
	16	100		1,70	1,20	0,70	0,45			
clay	8	130	SH 16 x 130	0,21	0,13	0,05	0			
hollow and	10	130	SH 16 x 130	0,21	0,13	0,05	0			
solid brick	12	130	SH 20 x 130	0,21	0,13	0,05	0			
(Hlz + Mz)	12	200	SH 20 x 200	0,21	0,13	0,05	0			
calcium silicate	8	130	SH 16 x 130	0,21	0,13	0,05	0			
hollow and	10	130	SH 16 x 130	0,21	0,13	0,05	0			
solid brick	12	130	SH 20 x 130	0,21	0,13	0,05	0			
(KSL + KS)	12	200	SH 20 x 200	0,21	0,13	0,05	0			

Table 5-1: Summary of the characteristic resistance against pullout or steel failure

<sup>1)</sup> applies for stainless steel A4

Date: 6<sup>st</sup> of November 2018

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